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## (54) Vaporizing heavy hydrocarbon feedstocks without coking

(67) A method for a vaporizing heavy hydrocarbon which avoids the formation of coke in the feed heaters and is useful in a process for upgrading and/or converting the heavy hydrocarbon to lighter products. Heavy hydrocarbon feedstock (10) is heated (12) to a temperature below its coking point, then mixed (at 20) with hydrogen (16) heated (at 18) to a temperature sufficient so that the hydrocarbon feedstock is vaporized without forming coke. Alternatively, the heavy hydrocarbon feedstock can be fractionated to provide a light IBP-550°F (288°C) liquid fraction, and a heavy 550-850°F (288 - 454°C) liquid fraction. The light fraction is mixed with hydrogen and heated to a temperature sufficiently high, so that upon being mixed with the heavy liquid fraction the latter is heated through its dry point and vaporized without coking. The resulting vaporized hydrocarbon is usually further heated before being fed to a reaction step, such as hydrodealkylation.

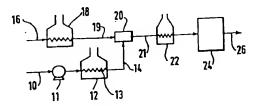
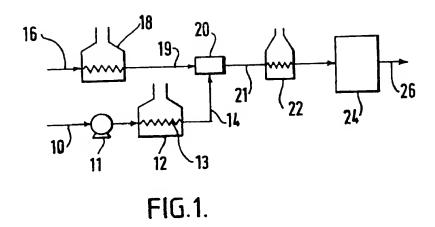


FIG.1.



 $\frac{12}{30}$   $\frac{12}{35}$   $\frac{14}{45}$   $\frac{13}{48}$   $\frac{13}{50}$   $\frac{13}{50}$   $\frac{13}{36}$   $\frac{13}{37}$   $\frac{14}{45}$   $\frac{13}{48}$   $\frac{13}{50}$   $\frac{13}{50}$   $\frac{13}{36}$   $\frac{13}{37}$   $\frac{14}{45}$   $\frac{13}{48}$   $\frac{13}{50}$   $\frac{13}{50}$ 

FIG.2.

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#### SPECIFICATION

# Vaporizing heavy hydrocarbon feedstocks without coking

5 This invention relates to the heating end vaporizing of heavy hydrocarbon feedstock materials. More particularly, it relates to e mathod for providing e vaporized heavy hydrocarbon feedstock which avoids the formation of coke in the feed heaters useful in e process for upgrading end/or converting the heavy hydrocarbon to lighter products, such as in e thermei hydrodealkylation process. One barrier to successful hydrodealkylation of heavy hydrocarbon aromatic materiels such as steam

10 crecker ter to produce mono-ring product materials is vaporization of the liquid phase feed material without producing excessive coke formation during the preheating step. It has generally been found that such heavy hydrocarbon liquids whan prehaetad to above 550°F (288°C) are susceptible to coking. To overcome this problem of undesired coke formation during preheating and to permit feeding heavier vaporized feedstock meterials to thermal or catalytic reaction processes, it has been found possible to make 15 use of superheated hydrogen and/or hydrocarbon vapours mixed with the heavy hydrocarbon feed to rapidly heat and vaporize the heavy hydrocarbon liquids to provids a vapor phase material without coking of the heavy hydrocarbon faed material. Although it is known in industry to use preheated hydrogen mixed with feed liquids upstream of a reaction step, such heated hydrogen has epparently not been previously used to vaporize hydrocarbon heavy feedstock materials which contain constituents which are 20 prone to coking in a conventional tubular fired heater preheating step.

This invention provides a method for providing a vaporized heavy hydrocarbon feedstock which avoids tha formation of coke in the feed heaters useful in a process for upgrading end/or converting the heavy hydrocarbon to lighter products, such as in e thermal hydrodealkylation process. The method comprises heating a heavy hydrocarbon feedstock to a temperature below its coking temperature, heating hydrogen 25 to a temperature sufficiently above the temperature of the heated hydrocarbon feedstock end hydrogen together, the heavy hydrocarbon feed material is completely vaporized without forming any coke.

in e second embodiment of the invention, e heavy hydrocarbon feedstock is first fractionated into e lighter fraction normally boiling below 550°F (288°C) and a heavier fraction having a normal boiling range of 550°F to 850°F(228 to 454°C). The heavier hydrocarbon fraction is heated to a temperature below its 30 coking point, and the lighter fraction and hydrogen are heated separately to a temperature below the coking point of the lighter fraction and sufficiently above the temperature of the heated heavy hydrocarbon fraction to provide a heat content sufficient that, upon being mixed with the heavy hydrocarbon frac-

tion, the latter is veporized without forming eny coke. Using this invention, the temperature of the mixing chambar wall can be mainteined at a significantly 35 lower traperature then would be required for the wall temperature of a tubuler type fired preheater for

veporizing the feedstock. This invantion for veporizing heavy hydrocarbon feedstocks is useful at a pressure range of 50-5000 psig (3.4-345 bar gauge). The veporized material stream can then be fed to a further reaction step auch ae hydrodeeikyletion to produce hydrodaalkylated products.

in the present invention for vaporizing heavy hydrocarbon feedstocks, so as to evoid formetion of coke, hydrogen is heeted to a temperature aufficient that upon mixing with the heavy hydrocarbon feedstocks will effectively heat same through their dry point and vaporize the heavy feedstock without coking. The heeted hydrogen is mixed with the heavy feedstock in a suitable mixing step such as a venturi mixer. The temperature of the heated hydrogen is much higher than the temperature of the heavy hydrocarbon

45 feed material, and is sufficiently high, such as 900-1250°F (482-677°C), that it supplies all the heat needed to vaporize the heavy ilquid feedstock, which normally boils above 550°F (288°C) end preferably hea a bolling range of 550-650°F (288-343°C). Because of the rapid heat transfer which occurs between the mixed streams in the mixing step, this heating method avoids transferring heat from a hot wall to the hydrocarbon feedstock and minimizes the time required to vaporize the heevy feed material and avoids

50 coking of the material. In a second embodiment of the Invention, tha hydrogen can be premixed with a light hydrocarbon fraction having a normal boiling range of 400-850°F (204-343°C) and heated together to a temperature below the coking point of the light hydrocarbon fraction and sufficient that, upon mixing with the heavy hydrocerbon feedstock fraction, will rapidly heet same through its dry point and completely vaporize the 55 heavy hydrocarbon feedstock without coking of the heavy hydrocarbon feedstock material.

This invention can be used for veporizing any hasvy hydrocarbon feed material for which e vepour phase reaction is required, such as for veporizing heavy gas olla and steam cracker tar derived from petroleum, and coal-derived liquids, prior to feeding the vaporized hydrocarbon material to a further reaction step such as thermal hydrocracking or hydrodealkylation to produce hydrodealkylation products. 60 Useful pressure ranges for the invention ere 50-5000 psig (3.4-345 bar gauge) and preferably 200-1000

paig (13.8-69 bar geuge). Reference is now made to the accompanying drawings, in which:

Figure 1 is a flow diagram illustrating a method for vaporizing a heavy hydrocarbon feedstock according to the present invention; end

Figure 2 is a flow diagram of a second embodiment of the method illustrated in Figure 1.

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As shown in the Figure 1 drawing, a heavy hydrocarbon feedstock material such as heavy gas oil, is provided at 10, pressurized at 11 to at least about 200 psig (13.8 bar gauge) and heated in furnace 12 to a temperature such as about 560°F (293°C), which will not produce coke deposits inside the tubes 13 of the furnace. The heated feedstock stream at 14 is passed to a mixing step at 20. Also, hydrogan gas is provided at 16 and heated in furnace 18 to a temperature well above temperature of the mixing step 20 and also passed via line 19 to the mixing step.

Mixing step 20 may comprises any suitable known mixing device which provides complete mixing at relatively high velocities, such as a length of pipe, nozzle or venturi, with the heavy oil stream 14 preferebly being introduced into the throat section of a venturi. The heat content provided in hydrogen stream 10 19 is sufficient to completely vaporize the heavy hydrocarbon feed stream 14, and thus avoids heating the hydrocarbon feedstock through its dry point by contact with a hot metal wall maintained at higher

temperature and thereby prevents any coking of the heavy feed material during such heating.

The resulting vaporized material at 21 is further heated in heater 22 to about 1250°F (677°C) and passed to a further reaction step 24, such as for a hydrodealkylation process, to produce a product 26.

in an alternative embodiment of the invention, as shown in Figure 2, a heavy feedstock material such as steam cracker tar is provided at 30 and fed into fractionation tower 32, which is usually maintained at operating conditions of about 200-300°F (93-149°C) temperature and 1-5 psia (0.069-0.345 bar absolute) pressure. From tower 32, a vapor stream can be withdrawn at 33, a light liquid stream boiling up to about 550°F (288°C) is withdrawn at 34, a heavy liquid stream having a boiling range of 550-850°F (288-20 454°C) is withdrawn at 36, and a heavier bottoma material boiling above about 850°F (454°C) is withdrawn at 38.

The light liquid stream 34 is pressurized at 35 to at least about 200 psig (13.8 bar gauga), hydrogen is added at 40 and hasted at 41, and the resulting mixture is heated in heater 42 to a temperature above about 950°F (510°C) and passed as stream 43 to mixing step 44, which can advantageously comprise a venturi mixing device having a reduced pressure and incressed flow velocity at its throat section. Tha heavy boiling liquid stream 36 is pressurized at 37 to at least about 200 psig (13.8 bar gauge), heated at 46 to a temperature sufficiently low to avoid coking in the tubes of heater 46, such as about 550°F (288°C), and also passed to the throst section of the venturi mixing step 44. The heat provided in atream 43 is sufficient to vaporiza ilquid stream 47, so that the resulting mixed stream which emerges at 45 from mixar 44 is completely vaporized. This vapor stream 45 is then passed through haster 48 for further heating such as to 1200-1250°F (649-677°C) temperature before passing to further reaction step 50, which may preferably be a hydrodealkylation stap. If the feedstock at 30 is a polynuclear aromatic or polyalkylated phenoi material, the light liquid stream at 34 can contain mainly alkylated nephthalene material, which is heated with hydrogen at 42 to a tamperature sufficient so that upon being mixed with the heated heavy 35 stream 47, which can be mainly alkylated phenanthrenea, the latter is completely vaporized. The resulting vaporized materiel is then fed to a hydrodealkylation reaction process step at 50 to produce product at 52.

This invention will be further described by reference to the following Examples, which should not be construed as limiting the scope.

### Example 1

To show the method and utility of the present Invention, a heavy hydrocarbon feed material such as gas oil normally boiling above about 600°F (316°C) temperature is pressurized to about 650 paia (45 bar gauga) pressure and heated to a temperature of at least 600°F (316°C) but balow which any coking of tha 45 feed occurs. The heated feed material is then vaporized by being mixed with a hydrogen stream heated to a temperature sufficiently above the mixing temperature to have a heat contant sufficient that, upon being mixed with the heavy liquid feed, will completely vaporize the feed with coking. The molar flow ratio of hydrogen to feed liquid is about 13, and the hydrogen stream contains 90% hydrogen and 10% methans. Results of the heating and mixing steps for various hydrocarbon feed stock fractions are shown 50. In Table 1.

### TABLE 1

Vaporizing hydrocarbon feedstock by mixing with heated hydrogen

<b>5</b> 5	Liquid Feedstock Avg. BP, *F(°C)	Liquid Feed Temp, °F(°C)	<i>H</i> ± Temp, °F(°C)	<i>Mixing</i> Tamp, °F(°C)	55
60	600 (316)	600 (316)	1000 (538)	690 (366)	60
	650 (343)	600 (316)	1125 (607)	735 (391)	
65	700 (371)	650 (343)	1250 (677)	803 (428)	65

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It is seen that the heavy hydrocarbon feed materials having average boiling points between 600 (316°C) and 700°F (371°C) can be heated and completed vaporized without coking by being mixed with a hydroge stream heated to a higher temperature but not exceeding 1250°F (677°C) to provide a hydrocarbon vapor material.

Example 2

A heavy hydrocarbon feed material such as steam cracker tar is fractionated into at least slight fraction having a normal boiling range of 300-550°F (149-288°C) and a hasvy fraction having a boiling range of 550-850°F (288-454°C). The heavy hydrocarbon fraction is heated to a temperature below its coking point 10 and passed to a mixing stap. The light fraction stream is mixed with heated hydrogen and the resulting stream is heated to a temperature higher than that of the heavy fraction and such as to provide a heat content sufficient that, upon mixing the two prehated hydrocarbon streams together, the heavy hydrocarbon stream is completely vaporized without any coking. Results of the heating and mixing steps for verlous hydrocarbon feedstocks at 650 pei (45 bar) using 13 moles hydrogen, 1 mole light hydrocarbon 15 fraction and 1 mole heavy hydrocarbon fraction feed are shown in Tabla 2.

TABLE 2

Vaporizing heavy hydrocarbon fraction by mixing with heated hydrogen and light hydrocarbon fraction

vap	ponzing neavy hydrocarbon macdon by mining				
20	Liquid Feedstock Avg. BP, 年 (°C)	Heavy Liquid Feed Temp, *F (*C)	<i>Light Liquid</i> and H₂ Temp, ℉ (℃)	Mixing * Temp, *F (*C)	25
25					
	600 (316)	600 (316)	1000 (638)	830 (443)	
30	650 (343)	600 (316)	1000 (538)	825 (441)	30
	700 (371)	600 (316)	1000 (538)	820 (438)	

Temperatures are ± 30°F.

It is seen that the heavy hydrocarbon feedstocks having initial boiling points between about 600-700°F (316-371°C) can be heated and completely vaporized without coking by being mixed with a light hydrocarbon liquid fraction and hydrogen mixture heated to a temperature sufficiently above the mixing temperature, but not exceeding about 1000°F (538°C), to heet and vaporize the heavy feedstock and provide a hydrocarbon vapor material.

#### 40 CLAIMS

- 1. A method for providing a vaporized heavy hydrocarbon feedstock which avoids the formation of coke in the feed heaters and is useful in a process for upgrading and/or converting said heavy hydrocar-
- 45 bons, said method comprising: (a) heating a heavy hydrocarbon feedstock to a temperature of at least 500°F (260°C) but below its cok
  - ing point; (b) heating hydrogen to a temperature sufficiently above the temperature of said heated heavy hydro-
- carbon feedstock so as to provide a heat content sufficient to vaporize said heated heavy hydrocarbon 50 feedstock; and (c) mixing said heated heavy hydrocarbon feedstock together with said heated hydrogen and vaporiz
  - ing the heavy hydrocerbon feedstock to provide a hydrocerbon vapour meterial without forming coke. 2. A method according to claim 1, wherein said heavy hydrocarbon feedstock is heated to a tampera-
- ture of 550-650°F (288-343°C). 3. A method according to claim 1 or 2, wherein said hydrogen is heated to a temperature of 1000-1260°F (538-677°C).
  - 4. A method according to any of cleims 1 to 3, wherein the heavy hydrocarbon feedstock is steem cracker tar derived from petroleum.
- 5. A method according to any of claims 1 to 3, wherein the heavy hydrocarbon feedstock is a coal-60 derived liquid.
  - 6. A method according to any of claims 1 to 5, wherein said mixing step occurs in a venturi device.
  - 7. A method according to any of claims 1 to 6, wharein the mixed and vaporized hydrocarbon material and hydrogen are further heated to a temperature above the vaporization temperature of said heavy hydrocarbon feedstock.
- 8. A method according to claim 7, wherein said heated mixture of vaporized hydrocarbon material